

TEMA 4: SISTEMAS DE TRANSMISIÓN DIGITAL PASO BANDA

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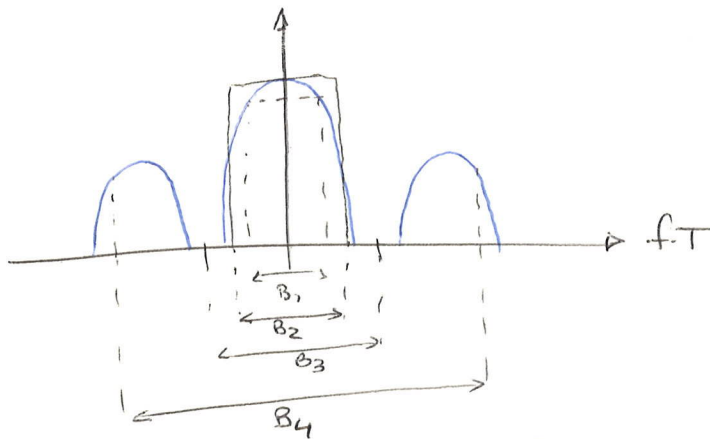
4.4.2- Criterios de diseño

4.1 - INTRODUCCIÓN

Vamos a ver modelaciones $\Rightarrow$ antenas más eficientes y multiplicación de información

Ancho de banda: distintas formas de medirlo

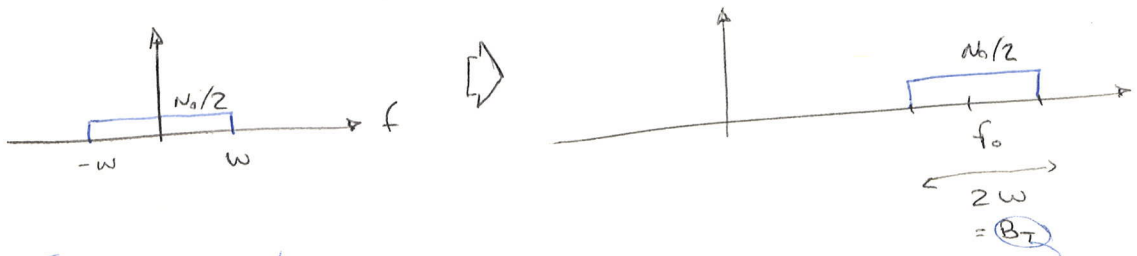
- A 3dB (B_1)
- Equivalente de ruido (B_2)
- De primeros nulos (B_3)
- Contenido de potencia fraccional (B_4)



Probabilidad de error: es función de G y SNR

$$\boxed{\text{SNR} = \frac{S}{N} = \frac{E_b \cdot R}{\frac{N_0}{2} \cdot 2B_T} = \frac{E_b}{N_0} \cdot \frac{R}{B_T}}$$

E_b = energía por bit (J/bit)



$$\frac{E_b}{N_0} \sim \text{dB/bit}$$

$$\frac{R}{B_T} \equiv \text{eficiencia espectral}$$

$$\boxed{\eta = \frac{R \text{ (bps)}}{B_T \text{ (Hz)}}$$

$\rightarrow$ anchura de banda de transmisión

Objetivos:

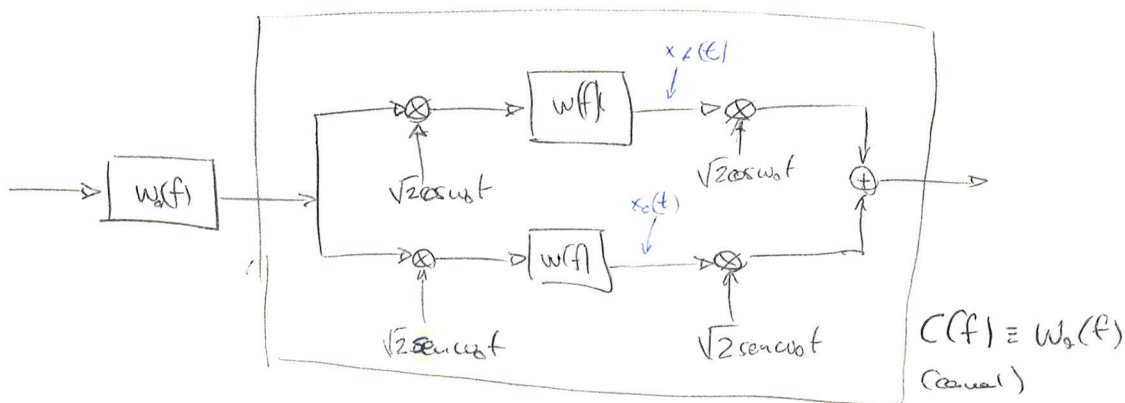
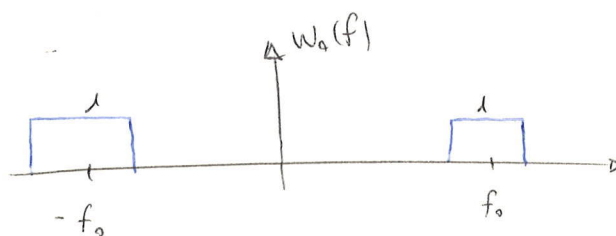
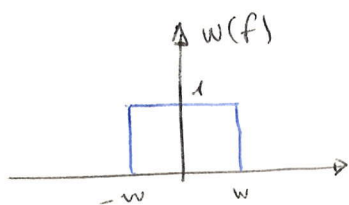
- 1.- Minimizar la probabilidad de error por bit (BER)
- 2.- Minimizar la potencia (P) requerida
- 3.- Maximizar la eficiencia espectral (η)
- 4.- Minimizar la complejidad

Objetivos incompatibles entre sí.

4.2- PLANTEAMIENTO GENERAL

Blau blau blau... Señal analítica y equivalente paso

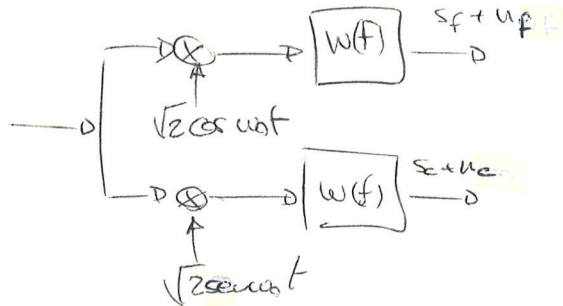
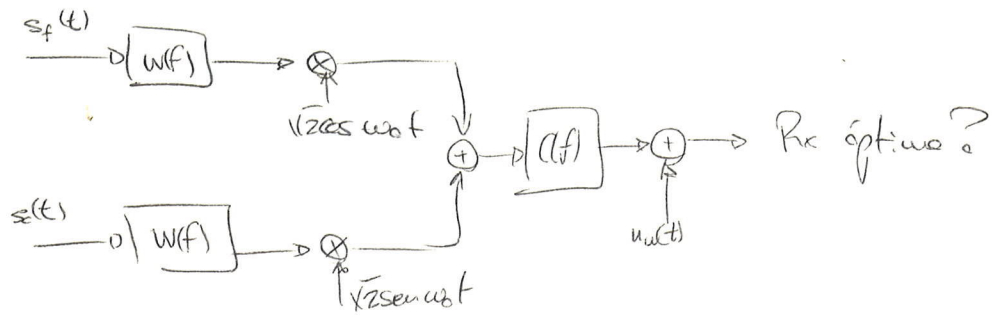
bajo... zzzzzz



$$x(t) = (x_f(t) \cos w_0 t + x_c(t) \text{sen } w_0 t) / \sqrt{2}$$



Es posible recuperar la información solo si consigo sincronizar.



$$u_w(t) = (u_f(t) \cos \omega_c t + u_z(t) \sin \omega_c t) \sqrt{2}$$

$\uparrow$
 $u_{fb}(t)$
fuera de banda

Conclusiones:

- 1.- Tenemos un canal doble (fase/cuadratura)
- 2.- No hay que cambiar la teoría para el Rx óptimo
- 3.- El ruido fuera de banda es irrelevante (6 filtros)
- 4.- Hay que garantizar el sincronismo

$b(t)$ es equivalente para bajo

$$x(t) = \text{Re} \left(b(t) e^{j\omega_c t} \right)$$

Teoría 1 $\rightarrow y(t) = \sum_n A(nT_s) \cdot b(t - nT_s)$

$$y(t) = \text{Re} \left(\sum_n \left(A_{kn}(nT_s) \right) b(t - nT_s) \cdot e^{j\omega_c t} \right)$$

Sólo vale para PAM

$$\rightarrow B_k(nT_s) + j C_n(nT_s)$$

4.3- TÉCNICAS DE MODULACIÓN DIGITAL

4.3.1 - PAM

(Pulse Amplitude Modulation)

4.3.1.1 - ASK-DSB

$$b(t) = b^R(t) + j b^I(t)$$

$$\text{En ASK-DSB, } \underline{b^I(t) = 0}$$

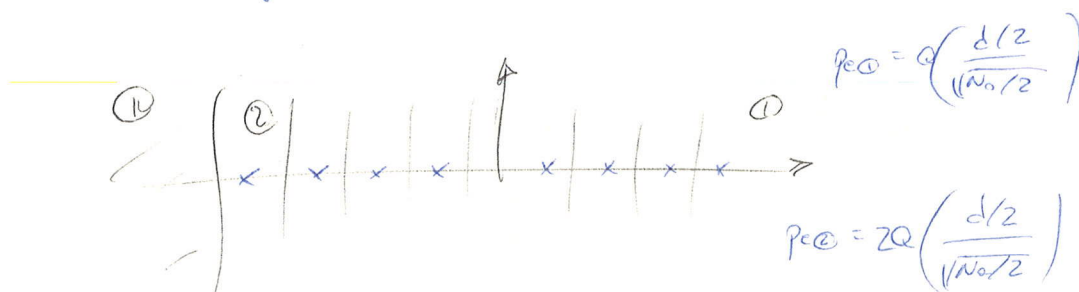
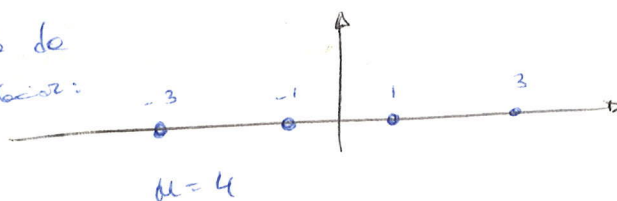
$$A_{k\mu}(\omega T_s) \in \mathbb{R}$$

$$A_{k\mu} = B_k = \frac{2K-1}{2} \cdot d \quad k \in \left\{1 - \frac{M}{2} + 1, \dots, \frac{M}{2}\right\}$$

$$y(t) = \operatorname{Re} \left(\sum_{\mu} B_k(\omega T_s) \cdot b^R(t - \mu T_s) \cdot e^{j\omega t} \right) =$$

$$= \left(\sum_{\mu} B_k(\omega T_s) \cdot b^R(t - \mu T_s) \right) \cos \omega_0 t$$

Ejemplo de
constelación:



$$p_e = 2 \left(1 - \frac{1}{M} \right) Q \left(\frac{d/2}{\sqrt{N_0/2}} \right)$$

$$E = E(d)$$

$$d = d(E)$$

$$E = \frac{d^2}{12} (M^2 - 1)$$

$$P_e = 2 \left(1 - \frac{1}{M}\right) \cdot Q \left(\sqrt{\frac{6}{M^2 - 1} \frac{E}{N_0}} \right)$$

E = energía media por símbolo

$$E = E_b \cdot \log_2 M$$

$$P_e = 2 \left(1 - \frac{1}{M}\right) \cdot Q \left(\sqrt{\frac{6}{M^2 - 1} \frac{E_b \cdot \log_2 M}{N_0}} \right)$$

$$\boxed{\eta = \frac{R}{B_T} = \frac{2W \cdot \log_2 M}{2W} = \log_2 M \text{ (bps/Hz)}}$$

$$P_{\text{trans}} = 2 \cdot W \quad (\text{caso ideal})$$

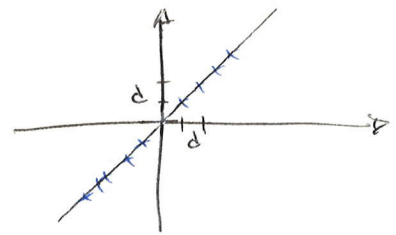
$$R = r \cdot H$$

$$M \uparrow \Rightarrow \left. \begin{array}{l} \eta \uparrow \\ P_e \uparrow \end{array} \right\} \rightarrow \text{compromiso}$$

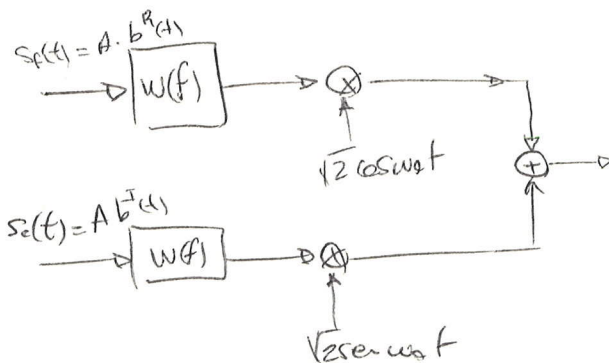
4.3.1.2 - ASK-SSB

$$b^{\pm}(t) = TH \} b^R(t) \} b^I(t)$$

Use menos bandas pero el sistema es más complejo.



Alora la distancia entre señales es $d\sqrt{2}$



$$P_e = 2 \left(1 - \frac{1}{M}\right) Q \left(\frac{d/\sqrt{2}}{\sqrt{N_0/2}} \right)$$

$$\boxed{P_e = 2 \left(1 - \frac{1}{M}\right) Q \left(\sqrt{\frac{3}{M^2 - 1} \cdot \frac{E_b}{N_0} \cdot 2 \log_2 M} \right)}$$

$$\boxed{\eta = \frac{2W \log_2 M}{W} = 2 \log_2 M \text{ (bps/Hz)}}$$

4.3.1.3 - QASK

Q = Quadrature

$$y(t) = \operatorname{Re} \left(\sum_n A_{kn}(\omega T_s) \cdot b(t - nT_s) \cdot e^{j\omega t} \right)$$

Suponemos $b(t)$ real y $A_{kn}(\omega T_s)$ complejos:

$$A_{kn}(\omega T_s) = B_k(\omega T_s) + j C_n(\omega T_s)$$

Hay M símbolos equiprobables ($\sqrt{M}$ niveles)

$$\begin{cases} B_k = \frac{2k-1}{2} d \\ C_n = \frac{2n-1}{2} d \end{cases} \quad k, n \in \left\{ -\frac{\sqrt{M}}{2} + 1, \dots, \frac{\sqrt{M}}{2} \right\}$$

Constelaciones cuadradas:

$$P_e = p(e/\omega_0) \cdot p_0 + p(e/\omega_2) \cdot p_2 + p(e/\omega_3) \cdot p_3$$

$$p(e/\omega_0) = 2Q\left(\frac{d/2}{\sqrt{M}/2}\right) - Q^2(\dots) \quad [\text{esquinas}]$$

$$p(e/\omega_2) = 3Q(\dots) - 2Q^2(\dots) \quad [\text{—}]$$

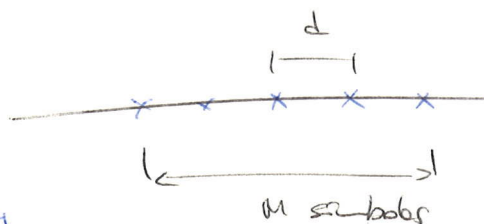
$$p(e/\omega_3) = 4Q(\dots) - 4Q^2(\dots) \quad [\square]$$

$$p_0 = \frac{4}{M} \quad p_2 = \frac{4(\sqrt{M}-2)}{M} \quad p_3 = \frac{(\sqrt{M}-2)^2}{M}$$

$$P_e = \frac{4}{M} (2Q - Q^2) + \frac{4(\sqrt{M}-2)}{M} (3Q - 2Q^2) + \frac{(\sqrt{M}-2)^2}{M} (4Q - 4Q^2)$$

Ahora tenemos la distancia en función de la energía. De ASK-DSB:

$$E = \frac{d^2}{12} (M^2 - 1)$$



Plano en horizontal hay $\sqrt{M}$ símbolos

$$E = \frac{d^2}{6} (M - 1) \rightarrow \frac{d/2}{\sqrt{N_0/2}} = \sqrt{\frac{3}{M-1}} \frac{E}{N_0}$$

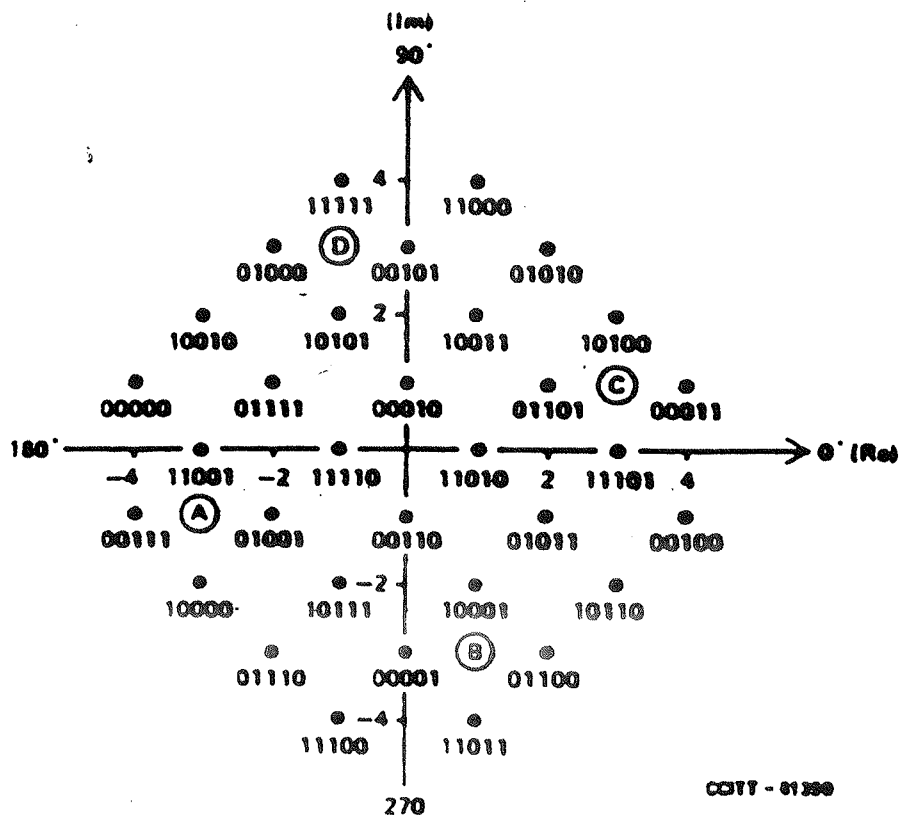
$$P_e = 4 \left(1 - \frac{1}{\sqrt{M}}\right) Q\left(\frac{d/2}{\sqrt{N_0/2}}\right) \left(1 - \left(1 - \frac{1}{\sqrt{M}}\right) Q\left(\frac{d/2}{\sqrt{N_0/2}}\right)\right)$$

Si SNR $\uparrow$, esto es despreciable

$$\rightarrow P_e \approx 4 \left(1 - \frac{1}{\sqrt{M}}\right) Q\left(\sqrt{\frac{3}{M-1}} \frac{E}{N_0}\right)$$

$$E = E_b \log_2 M$$

La p_e de símbolos: $p_e \approx 4 \left(1 - \frac{1}{\sqrt{M}}\right) Q\left(\sqrt{\frac{3}{M-1}} \frac{E_b}{N_0} \log_2 M\right)$



Los números binarios representan $Y0_n, Y1_n, Y2_n, Q3_n, Q4_n$

FIGURA 3/V.32

Constelación de señal de 32 puntos con codificación en rejilla para 9600 bit/s
y subconjunto de estados A, B, C y D utilizados a 4800 bit/s
y para el acondicionamiento

*Amplitudes de modulación de amplitud
y de fase*

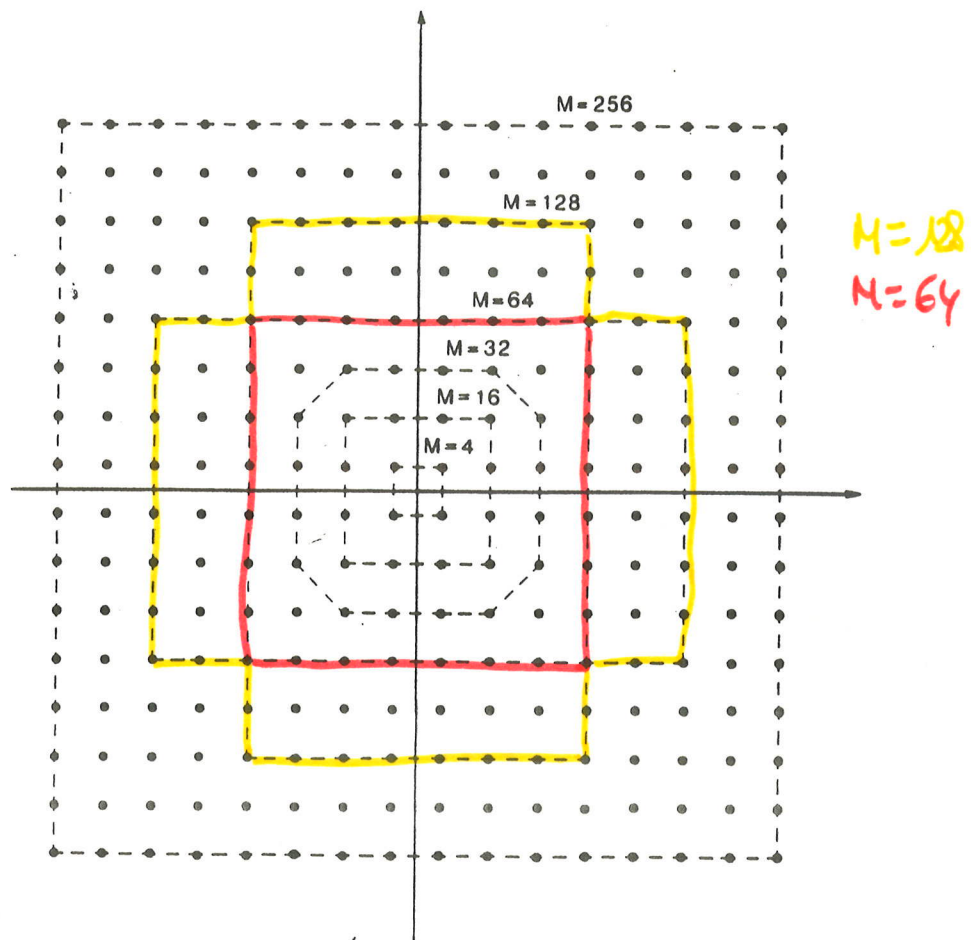


Figure 5.22 Rectangular AM-PM signal constellations. The dotted lines delimit the region of the signal points pertaining to that particular M . Notice the cross constellations for $M = 32 = 2^5$ and $M = 128 = 2^7$.

$$\eta = \frac{R(\text{bps})}{B_T(\text{Hz})} = \frac{r \log_2 M}{B_T}$$

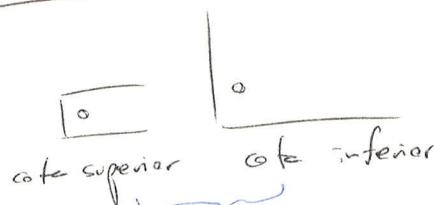
$$= \log_2 M \quad \text{¿por qué?}$$

▷ en la base, $1/B_T = 2$, al
modular B_T se duplica $\Rightarrow 1/B_T = 1$
(idealmente)

4.3.1.5 - ASK+PSK (AM-PM)

(transparencia rejilla)

Seguimos dando vueltas:



▷ funciona mejor que la
de Arthur's ...

4.3.1.4 - PSK (ooooo(eⁱ))

$$A_{kn} = \sqrt{E} \cdot e^{i \frac{2\pi K}{M}}$$

$$Q \left(\frac{\sqrt{E} \sin \pi/M}{\sqrt{N_b/2}} \right) < p_e < 2Q \left(\frac{\sqrt{E} \sin \pi/M}{\sqrt{N_b/2}} \right)$$



$$Q \left(\sin \pi/M \sqrt{\frac{2E_b}{N_0} \log_2 M} \right) < p_e < 2Q \left(\sin \frac{\pi}{M} \sqrt{\frac{2E_b}{N_0} \log_2 M} \right)$$

pe de simulado

$$\left| \frac{p_e}{\log_2 M} \leq \text{BER} \leq p_e \right|$$

$$\eta = \log_2 M \text{ (bps/Hz)}$$

4.3.2 - FSK

$$s_k(t) = \sqrt{\frac{2E}{T}} \cdot b(t) \cdot \cos(\omega_0 + \omega_k)t \quad 0 \leq t \leq T$$

$$\langle b^2(t) \rangle = 1$$

$$\omega_k = 2\pi f_k, \quad f_k = \frac{2k-1}{2} f_d$$

$$k \in \left\{ -\frac{M}{2} + 1, \dots, \frac{M}{2} \right\}$$

$$\cos \omega t$$

$$\cos(\omega + \Delta\omega)t \quad \left\{ \begin{array}{l} 0 = \int_0^T \cos \omega t \cdot \cos(\omega + \Delta\omega)t dt \end{array} \right.$$

ortogonales

$$\cos A + \cos B = 2 \cos \frac{A+B}{2} \cos \frac{A-B}{2}$$

$$A = (2\omega + \Delta\omega)t$$

$$B = \Delta\omega t$$

$$0 = \int_0^T \cos(2\omega + \Delta\omega)t \, dt + \int_0^T \cos \Delta\omega t \, dt$$

$$\Rightarrow \frac{\sin(2\omega + \Delta\omega)T}{2\omega + \Delta\omega} + \frac{\sin \Delta\omega T}{\Delta\omega} = 0$$

$2\omega + \Delta\omega$ es muy grande

$$\sin \Delta\omega T = 0 \Leftrightarrow \Delta\omega T = k \cdot \pi \quad k \in \mathbb{Z}$$

$$\boxed{Af \cdot T = k/2}$$

ortogonalidad de dos tons, siempre que la diferencia de fases sea cero.

$$\boxed{f_k = \frac{2k-1}{2} f_d, \quad f_d T = \frac{k}{2}}$$

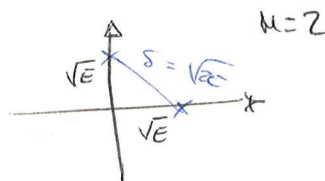
$$P_e \leq (M-1) \cdot P_e [M=2]$$

$$P_e [M=2] = Q\left(\sqrt{\frac{E}{N_0}}\right)$$

$$P_e \leq (M-1) \cdot Q\left(\sqrt{\frac{E}{N_0}}\right)$$

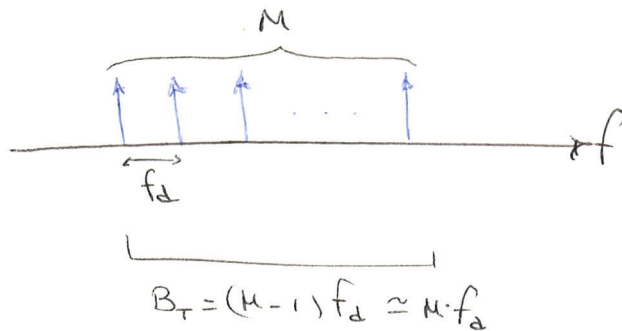
$$= (M-1) \cdot Q\left(\sqrt{\frac{E_b}{N_0} \log_2 M}\right)$$

para una constelación ortogonal.



Eficiencia espectral:

$$\eta = \frac{R(\text{bps})}{B_T}$$



$$\eta \approx \frac{\frac{1}{T} \log_2 M}{M \cdot f_d} = \frac{1}{f_d \cdot T} \cdot \frac{\log_2 M}{M}$$

En el mejor caso posible, $K=1 \rightarrow f_d \cdot T = 1/2 \rightarrow$

$$\rightarrow \eta \approx \frac{2 \log_2 M}{M} \text{ bps/Hz}$$

Si $M \uparrow$ $\left\{ \begin{array}{l} \eta \downarrow \\ E^{\text{tr}}, p_e \downarrow \end{array} \right.$

Para una constelación binaria, FSK ortogonal no es lo mejor posible.

Ejemplo:

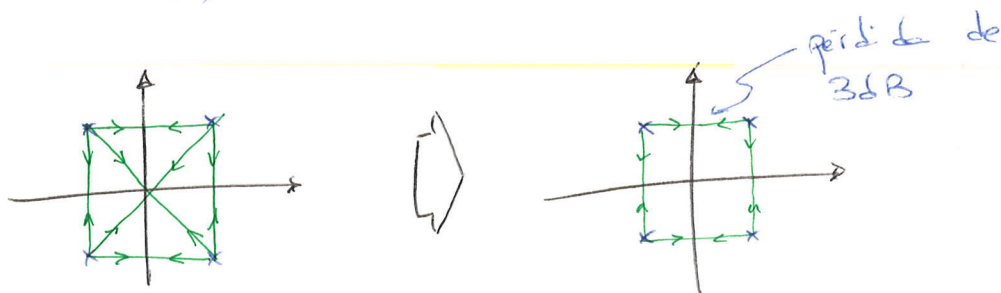
Averiguar la distancia entre 2 tones según su diferencia de frecuencias.

4.3.3- OTRAS TÉCNICAS

4.3.3.1 - QPSK

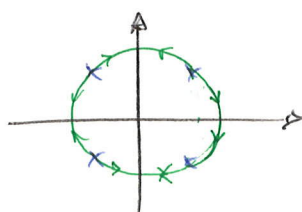
$Q \equiv$ offset

Prevenir las transiciones de 180° (que implican que en algún momento la potencia se hace cero).



4.3.3.2 - MSK (Minimum Shift Keying)

Se le da una forma a las señales para que las transiciones sean suaves.



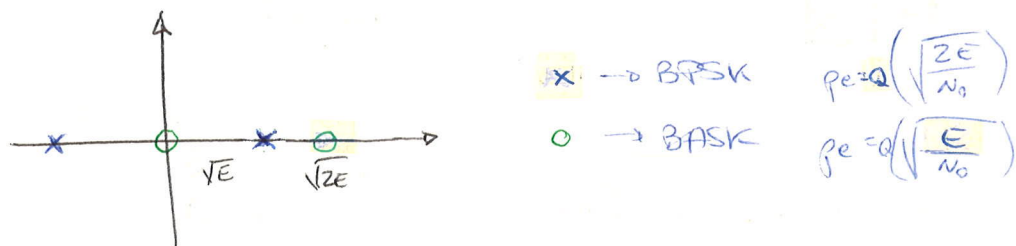
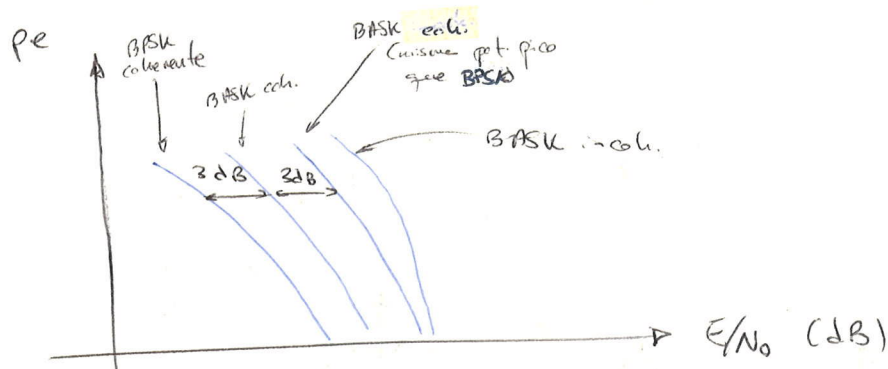
4.3.3.3 - DPSK

Resolver el problema de la determinación de la fase, transmitiendo la información en los cambios de fase.

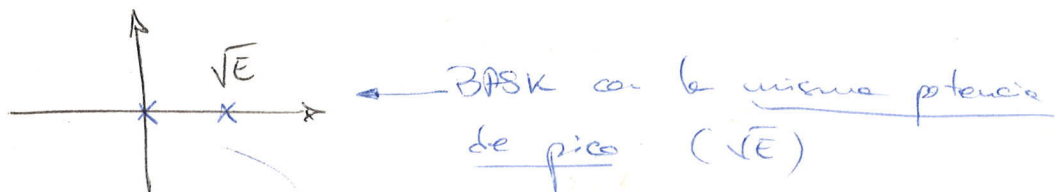
Las prestaciones son algo inferiores a PSK, pero permite la transmisión en canales no coherentes. Son inferiores porque, al ser un sistema con memoria, los errores se propagan.

4.4 - PRESTACIONES

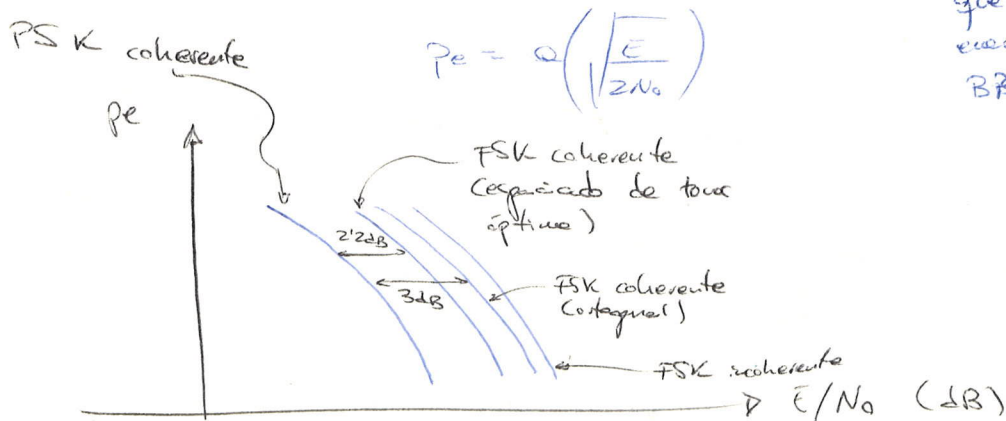
4.4.1 - COMPARACION DE SISTEMAS



BASK es la misma energía media es 3 dB peor



simbolos 3 dB más cerca $\Rightarrow$ sistema 3 dB peor que BPSK con misma energía media que BPSK



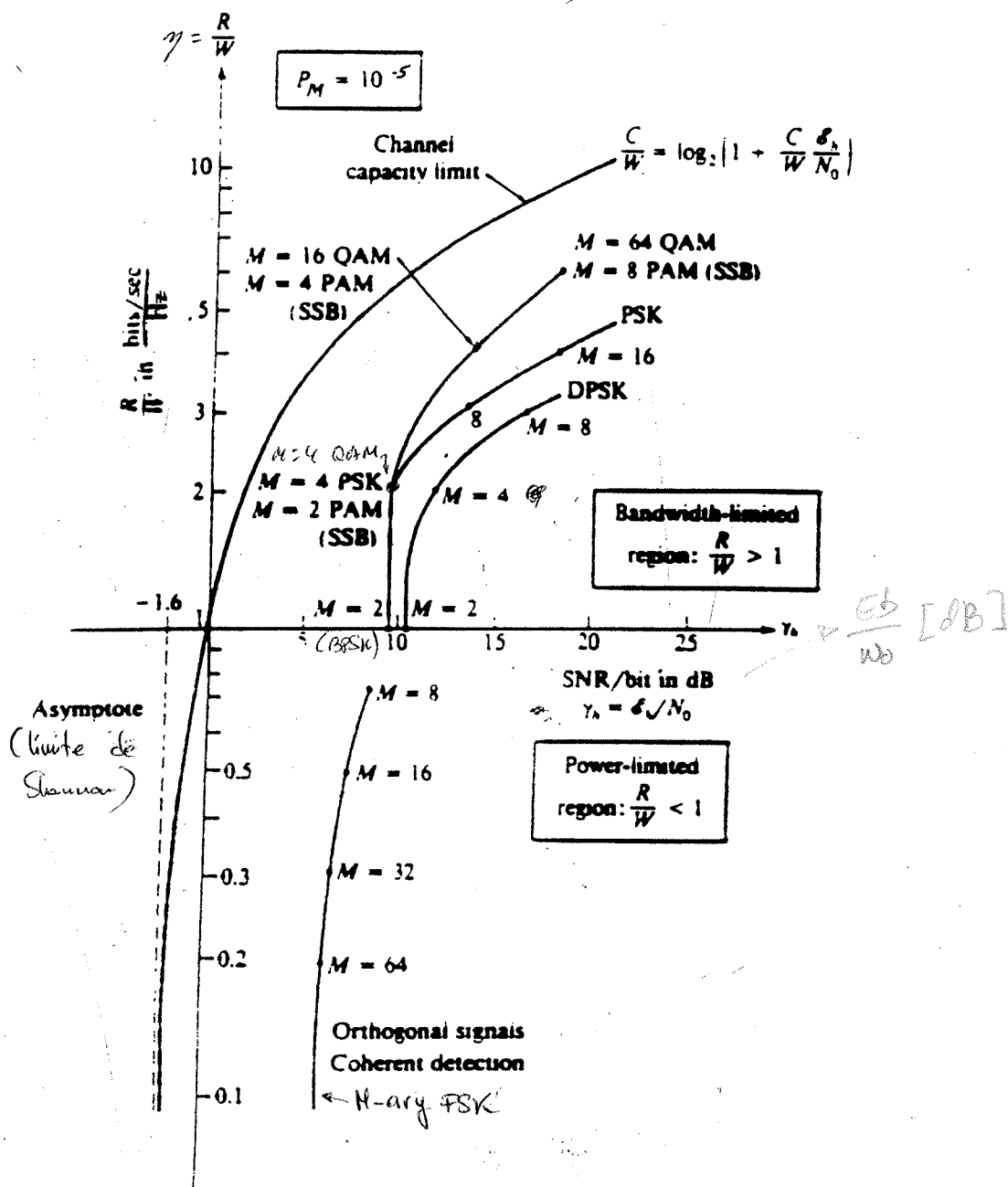


FIGURE 4.2.29

Comparison of several modulation methods at 10^{-5} symbol error probability.

LA transparence

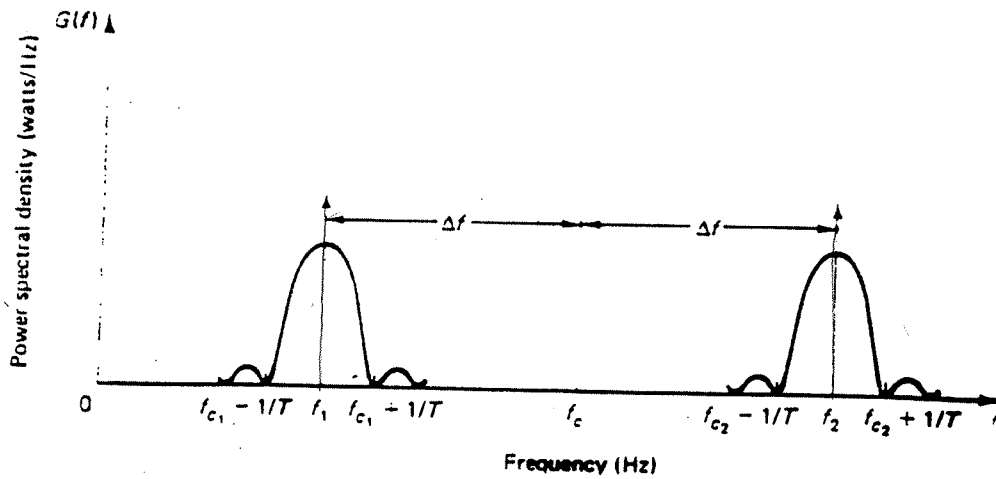


Figure 8.49 Power spectral density for BFSK.

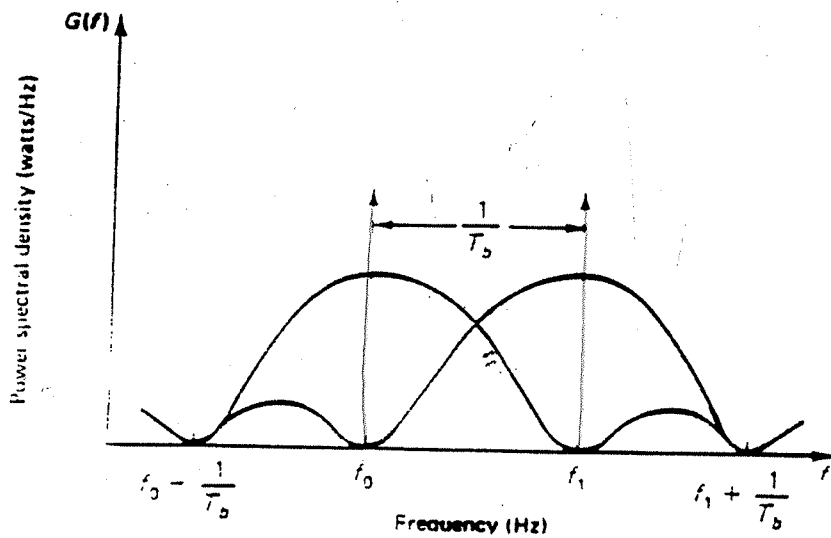


Figure 8.50 Power spectral density for BFSK, orthogonal tone spacing.

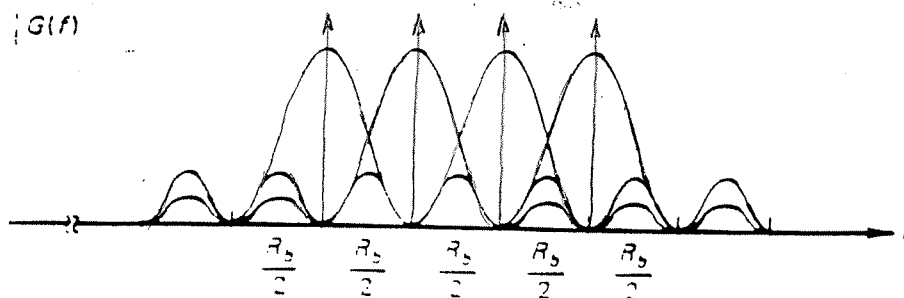


Figure 8.56 Power spectral density for 4-ary FSK.

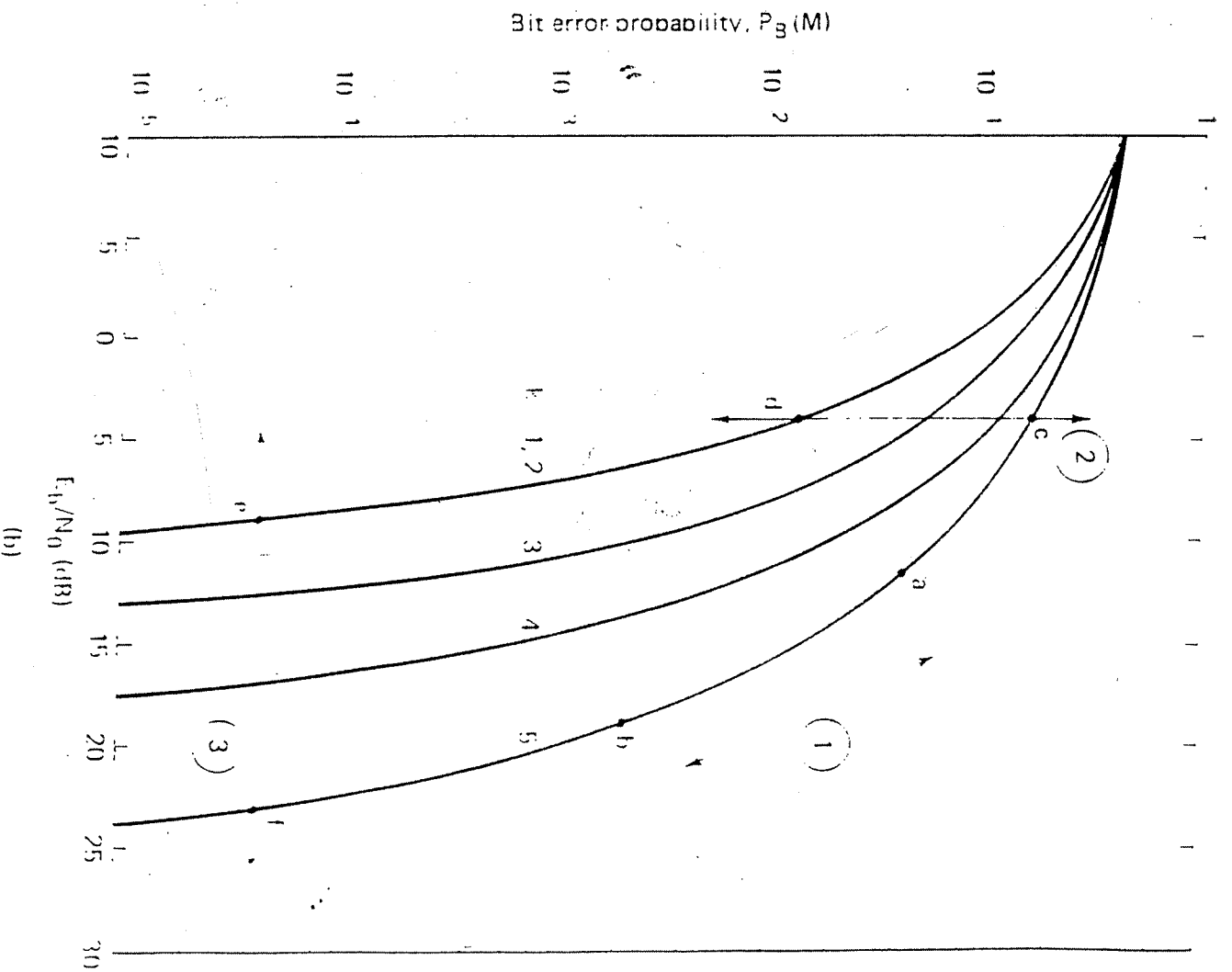
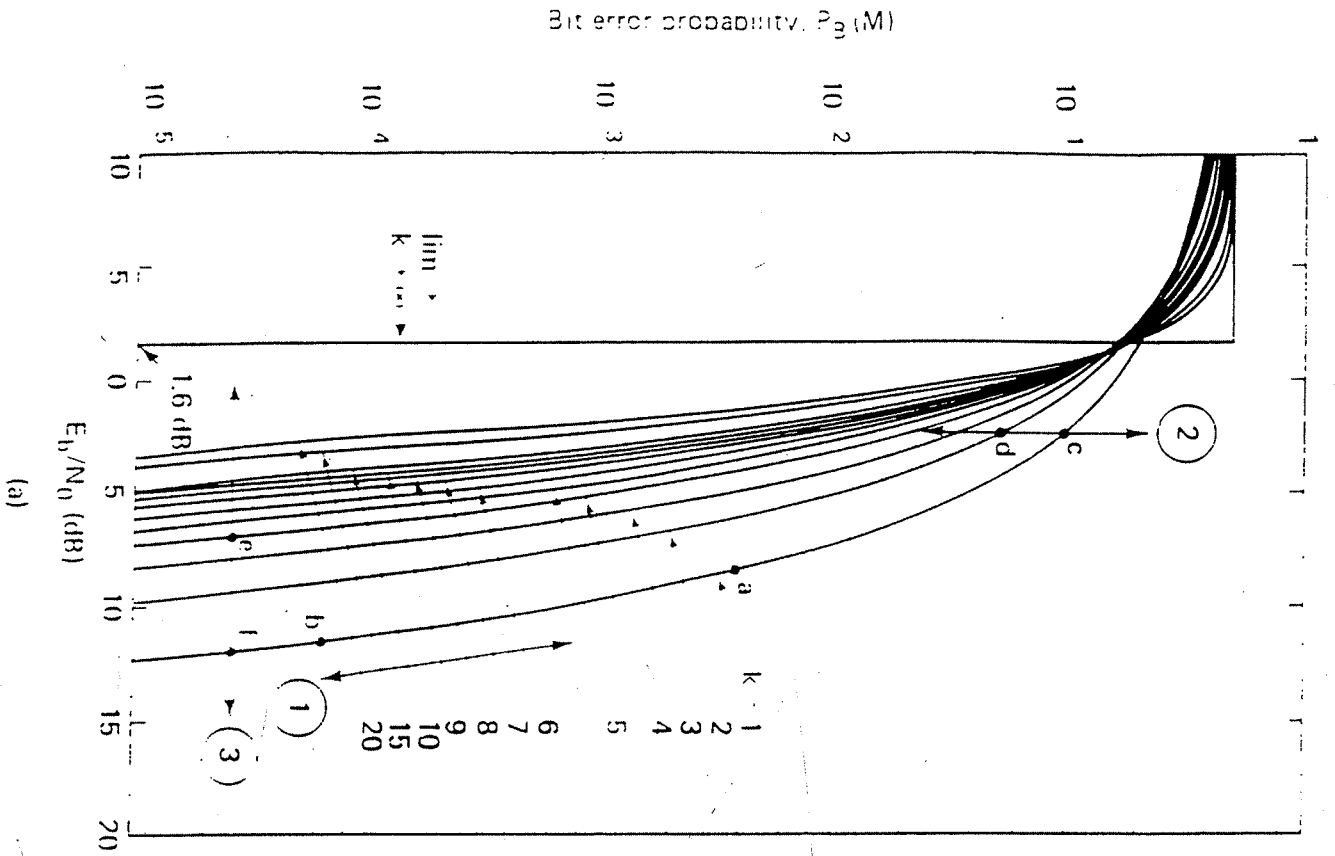
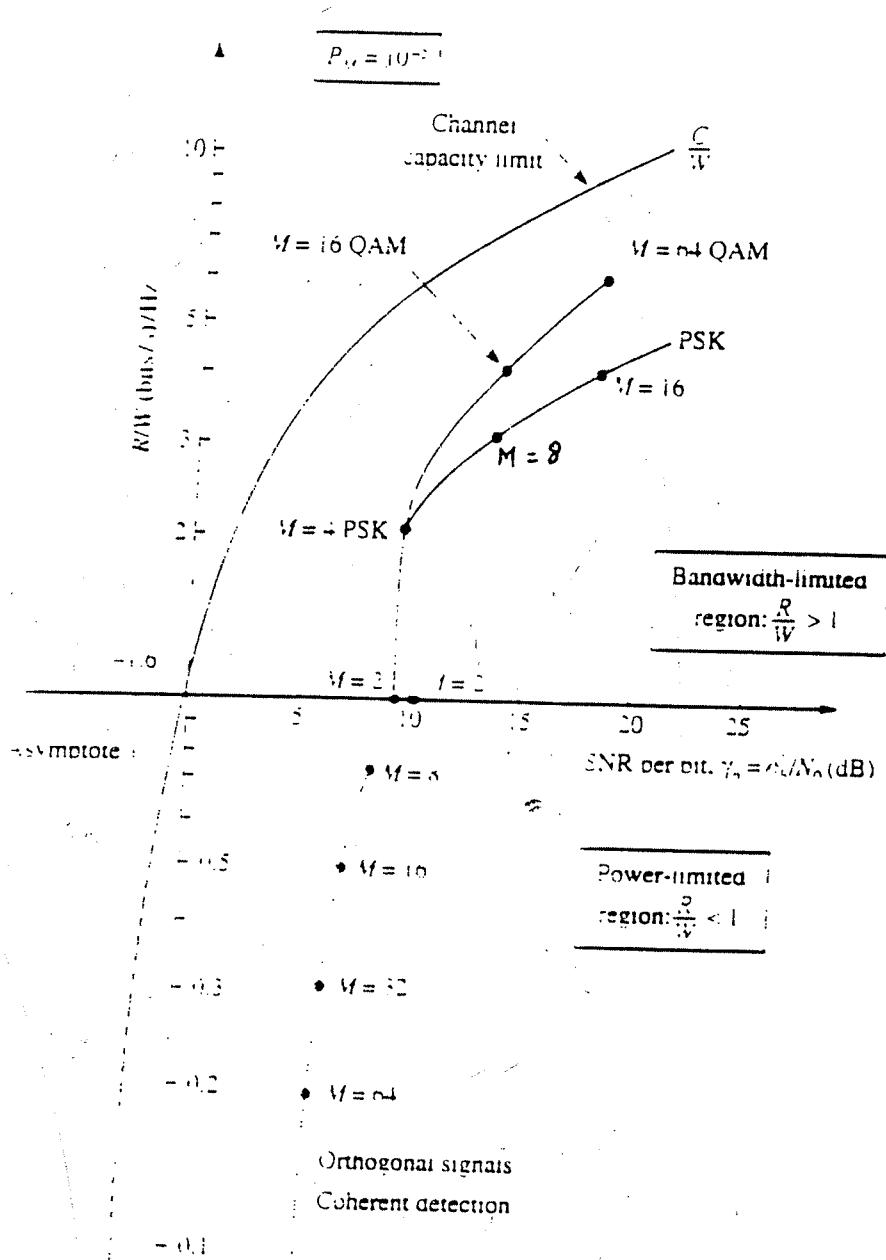


Figure 7.1 Bit error probability versus E_b/N_0 for coherently detected M ary signaling. (a) Orthogonal signaling. (b) Multiple phase signaling.



2-17 Comparison of several modulation methods at 10^{-5} symbol error probability

4.4.2- CRITERIOS DE DISEÑO

- Coste
- Complejidad
- R (bps)
- BER máxima
- B_T máxima
- P_T máxima
- P_{Rx}
- Tiempo de adquisición máxima del R_x

PROBLEMAS

- ① ¿Puede formarse una señal ASK sobre una portadora de 1MHz mediante la mezcla de la información con una onda periódica triangular de 500kHz? ¿Y de 200kHz?

Los armónicos pares no aparecen $\Rightarrow$ no se puede.

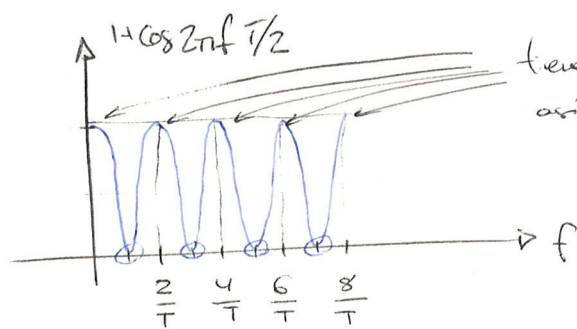
Si $x(t - T/2) = -x(t)$, los armónicos pares no aparecen.

$$X(f) \cdot e^{-j2\pi f \frac{T}{2}} = -X(f)$$

$$\Rightarrow X(f) (1 + e^{-j2\pi f \frac{T}{2}}) = 0$$

$$\Rightarrow \text{módulo} \quad |1 + \cos 2\pi f T/2 - j \sin 2\pi f T/2| = \sqrt{2(1 + \cos 2\pi f T/2)}$$

$$x(f) \cdot \sqrt{2(1+\cos 2\pi f T/2)} \cdot e^{j\theta} = 0$$



tiene que ser cero el producto,
así que $x(f)$ es cero

Si la portadora es de 200 kHz, el 5° armónico si
lo podemos sacar.

② a) Receptor óptimo de complejidad mínima

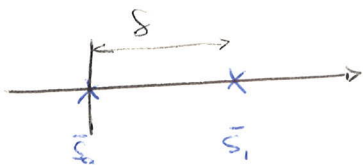
$$s_0(t) = a \quad s_1(t) = \sin(1000t + \theta)$$

Qual AWGN, $p_0 = 1/4$

b) Hallar p_1 si $N_0/2 = 10^{-3}$ W/Hz y $R = 100$ bps

c) EBW de primer sub?

Duración de $\bar{s}_i$:



$$100 \text{ bps} = 100 \text{ señales/s} \rightarrow T = 0.01 \text{ s}$$

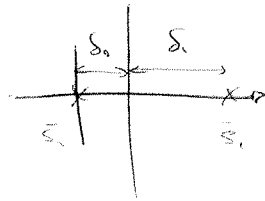
$$R = r(\text{baudios}) \cdot H(\text{bits/símbolo})$$

$$H = p_0 \log_2 \frac{1}{p_0} + p_1 \log_2 \frac{1}{p_1} =$$

$$100 = r \cdot \delta \quad \delta = 123.18 \text{ baudios} \\ = 1/T$$

$$= 0.81 \text{ bits/símbolo}$$

$$T = 0.0081 \quad \delta^2 = T/2$$



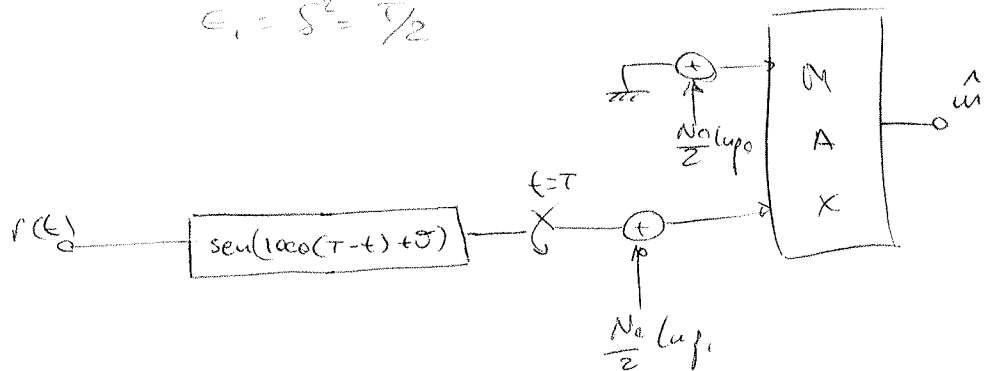
$$p_e = p_0 \cdot Q\left(\frac{s_0}{\sqrt{N_0/2}}\right) + p_1 \cdot Q\left(\frac{s_1}{\sqrt{N_0/2}}\right)$$

$$\begin{cases} s_0 = \frac{s}{2} + \frac{N_0}{2s} \ln \frac{p_0}{p_1} \\ s_1 = \frac{s}{2} + \frac{N_0}{2s} \ln \frac{p_1}{p_0} \end{cases}$$

$$a) \hat{u} = \max_i \left((\hat{r}_i, \hat{s}_i) - \frac{1}{2} E_i + \frac{N_0}{2} \ln p_i \right)$$

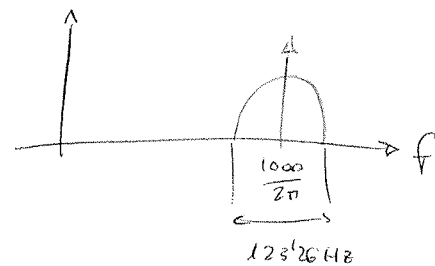
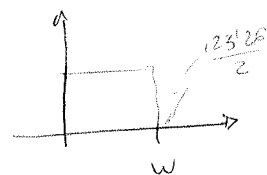
$$E_0 = 0$$

$$E_1 = s^2 = T/2$$



$$c) r = 123126 \text{ baud/s}$$

$$r_{\text{max}} = 2W \text{ en bande base}$$



④ Mensajes equiprobables, canal AWGN:

$$s_1(t) = \cos \omega t \quad s_2(t) = \cos(\omega + \Delta\omega)t$$

$$T = 1 \mu s$$

$$f = 1 \text{ MHz}$$

$$\Delta f = 250 \text{ Hz}$$

$$N_b/2 \text{ tal que } E/N_0 = 6$$

Calcular P_e . También si $\Delta f = 500 \text{ Hz}$

$$\int_0^T \cos \omega t \cos(\omega + \Delta\omega)t dt \approx \frac{T}{2} \sin 2\Delta f T = 0$$

despreciando el término
de frecuencia doble

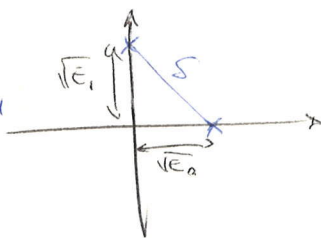
$$\Rightarrow 2\Delta f T = k \quad \Delta f \cdot T = k \quad k \in \mathbb{Z}$$

$$\Delta f_1 = 250 \text{ Hz} \Rightarrow \Delta f \cdot T = 1/4 \rightarrow \text{señales no ortogonales}$$

$$\Delta f_2 = 500 \text{ Hz} \Rightarrow \Delta f \cdot T = 1/2 \rightarrow \text{ortogonales}$$

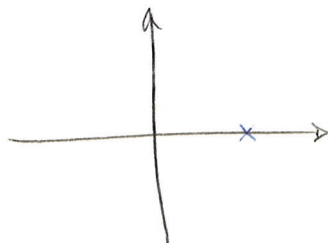
Caso 2:

$$\bar{E}_0 = \frac{1}{2} \cdot 1 \mu s = 5 \cdot 10^{-4} = \bar{E}_1 = \bar{E}$$



$$P_e = Q\left(\frac{S/2}{\sqrt{N_0/2}}\right) = Q\left(\sqrt{\frac{E}{N_0}}\right) = Q(\sqrt{6})$$

Caso 1:



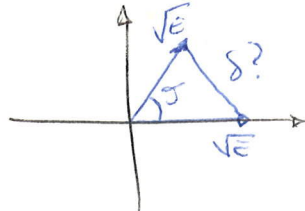
P_e caso
(Gaussian-Schmidt)

$$(x, y) = \|x\| \cdot \|y\| \cdot \cos \theta$$

$$= \sqrt{\frac{T}{2}} \sqrt{\frac{T}{2}} \cdot \cos \theta = \frac{T}{2} \sin c 2 \Delta f T$$

$$\cos \theta = \sin c 2 \Delta f T$$

$$= \sin \frac{1}{2} = \frac{\sin \pi/2}{\pi/2} = \frac{2}{\pi}$$



Teorema del coseno: $S^2 = E + E - 2E \cdot \cos \theta$

$$= 2E \cdot \left(1 - \frac{2}{\pi}\right)$$

etc.

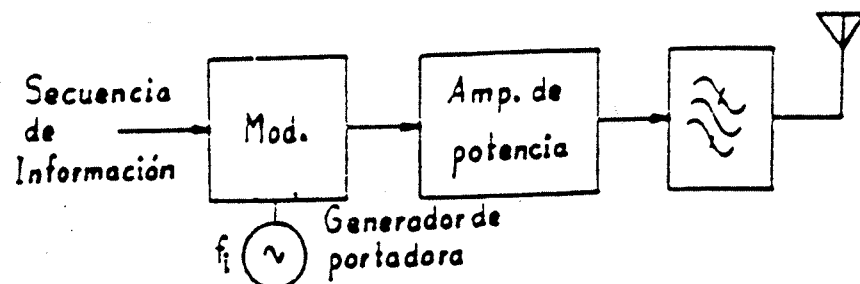


Figura 8.11. Transmisor PSK.

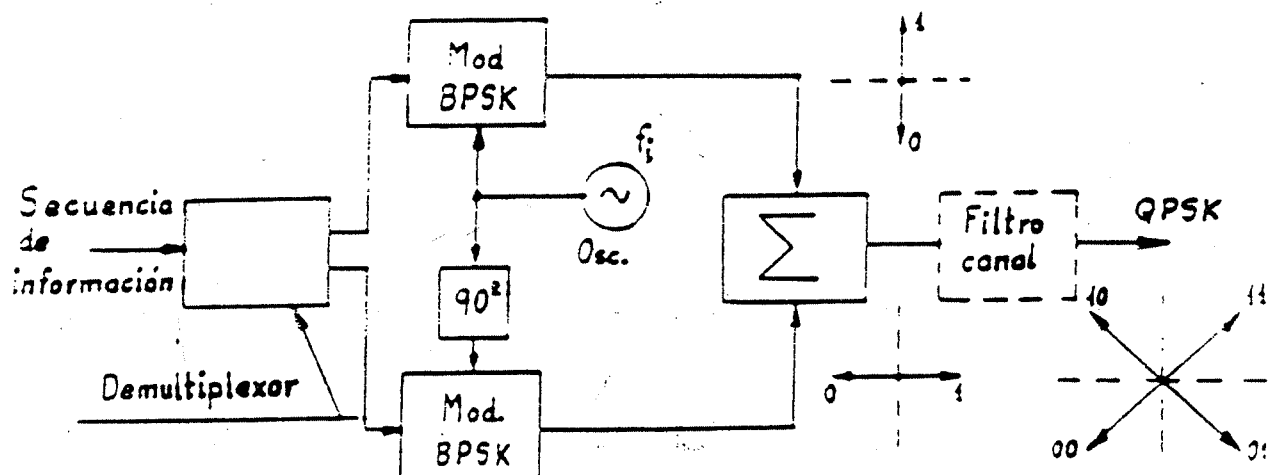


Figura 8.13. Modulador QPSK.

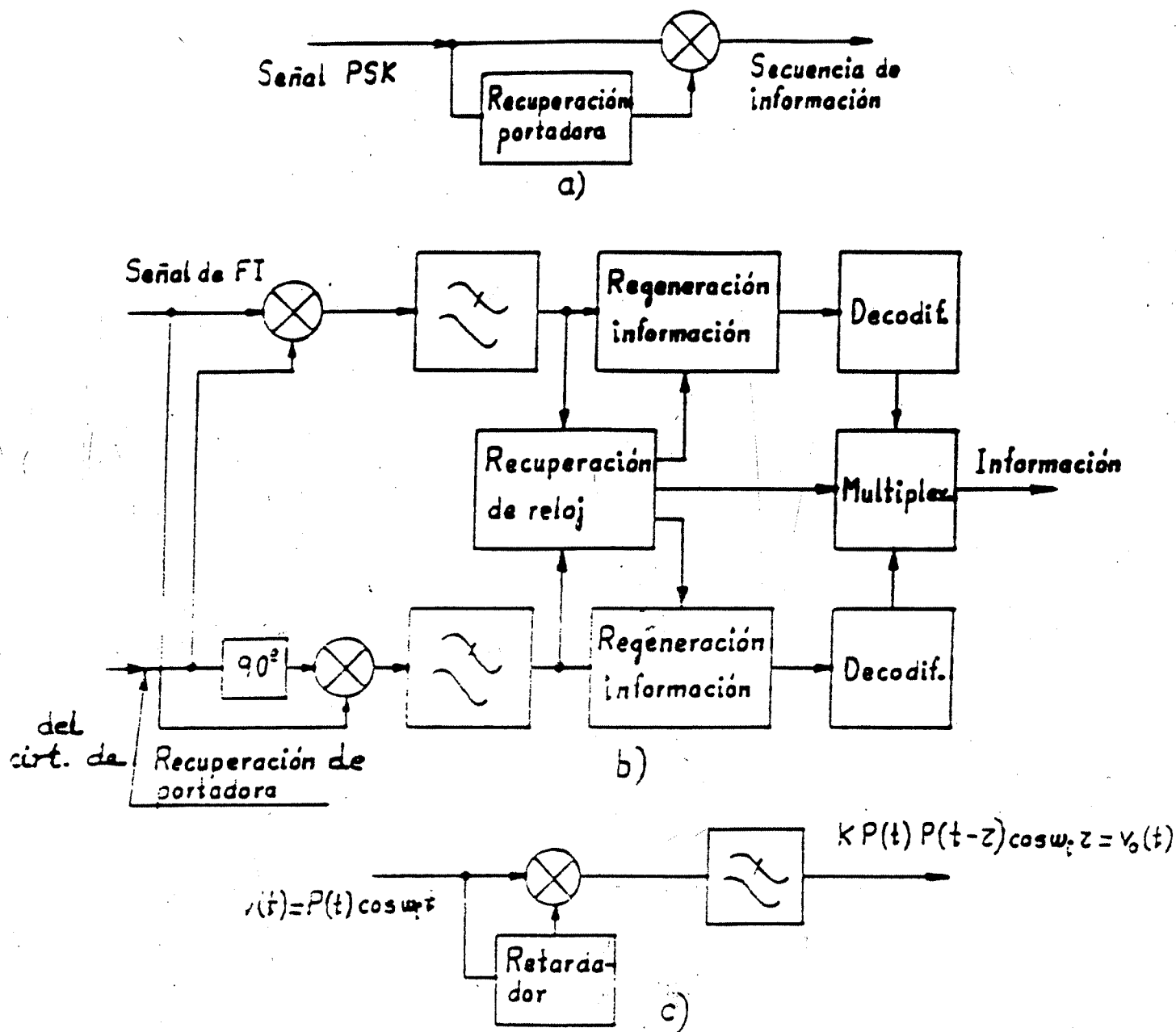
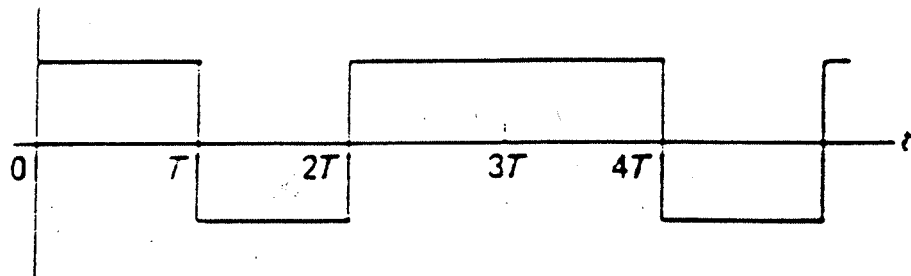


Figura 8.16. a) Detector coherente de BPSK
 b) Detector coherente de QPSK
 c) Detector Diferencial

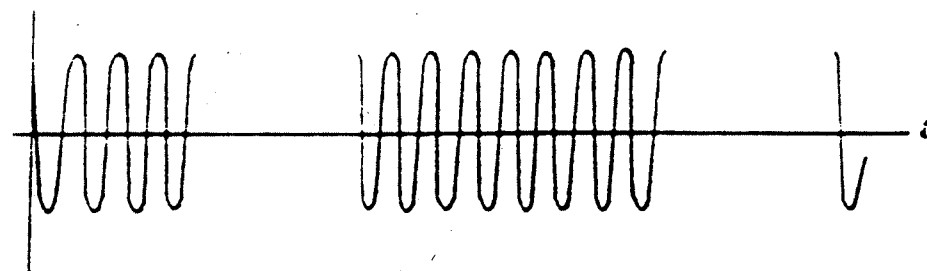
Digital
sequence:

1 0 1 1 0

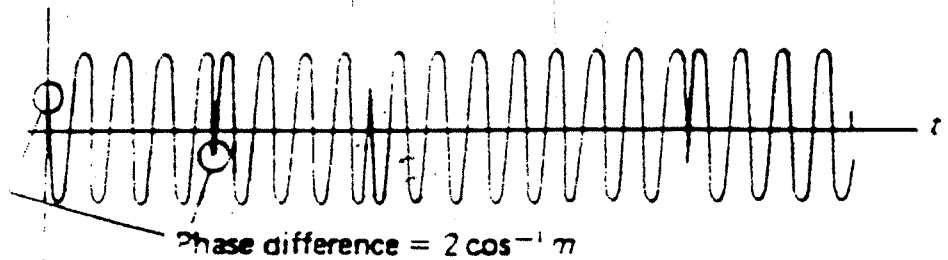
Antipodal
baseband
signal:



ASK:



PSK:



FSK:

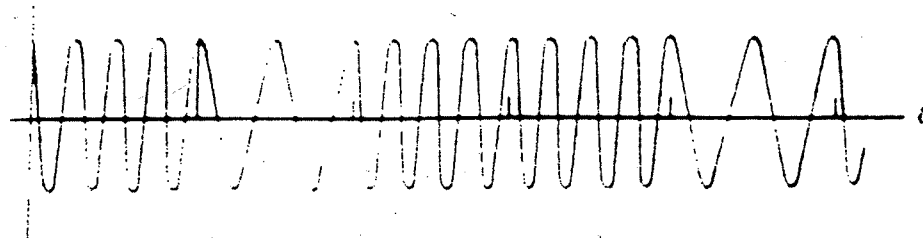


FIGURE 7.14 Waveforms for ASK, PSK, and FSK modulation

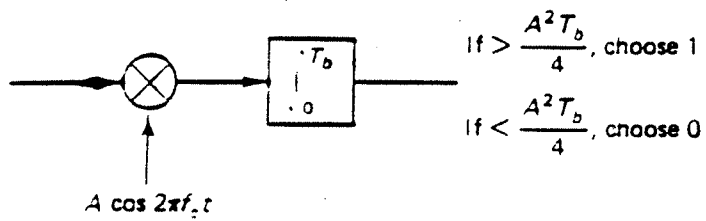


Figure 8.43 Matched filter detector for OOK.

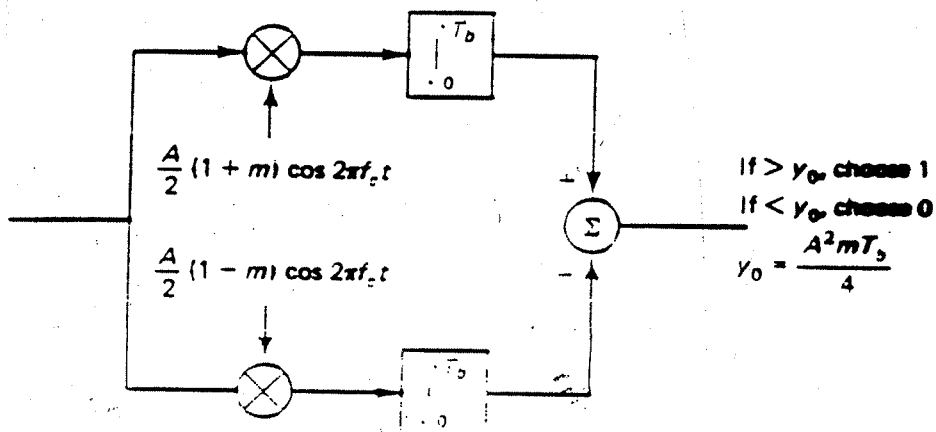


Figure 8.42 Matched filter detector for BASK.

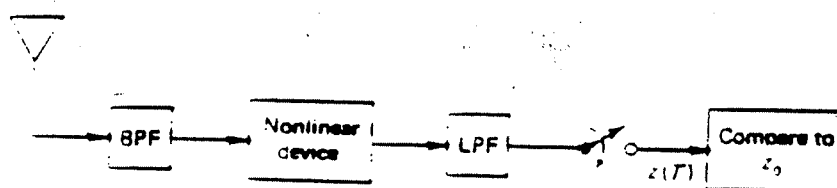


Figure 8.44 Envelope detector for OOK BASK.

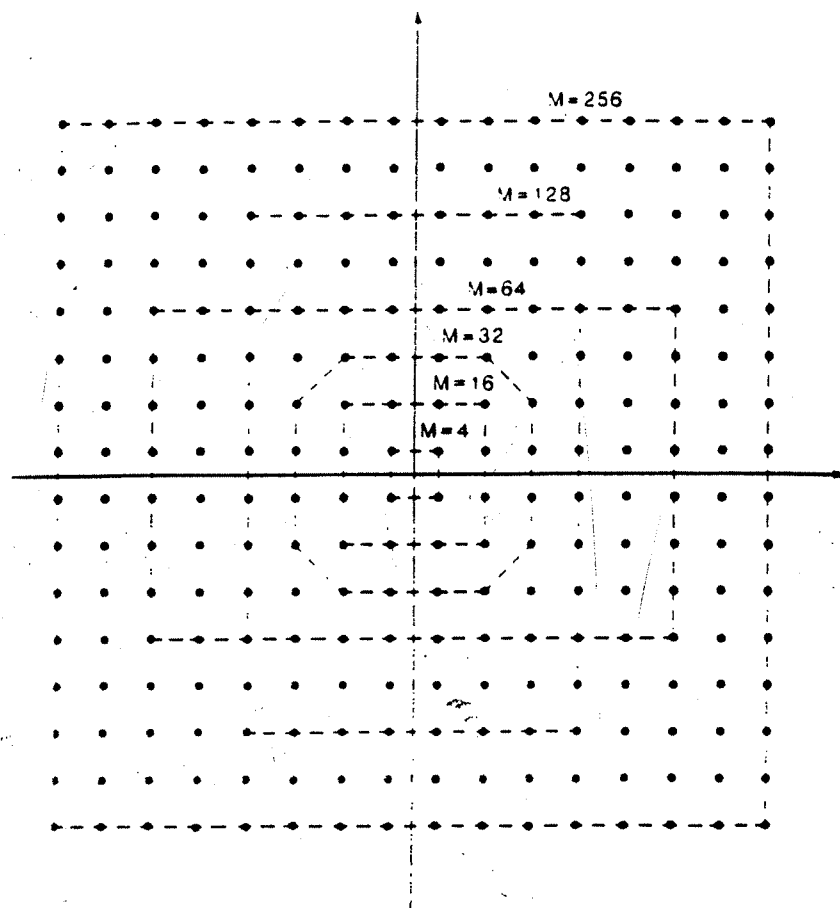


Figure 5.22 Rectangular AM-PM signal constellations. The dotted lines delimit the region of the signal points pertaining to that particular M . Notice the cross constellations for $M = 32 = 2^5$ and $M = 128 = 2^7$.

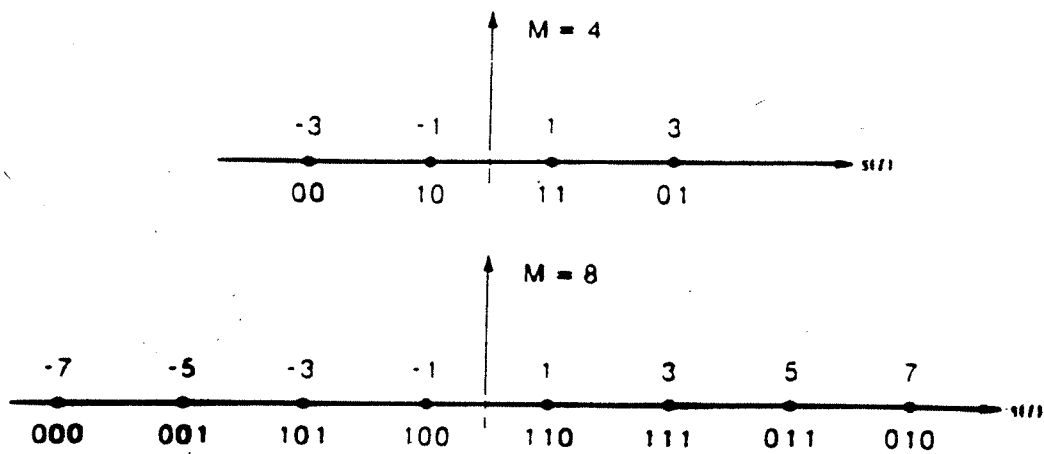
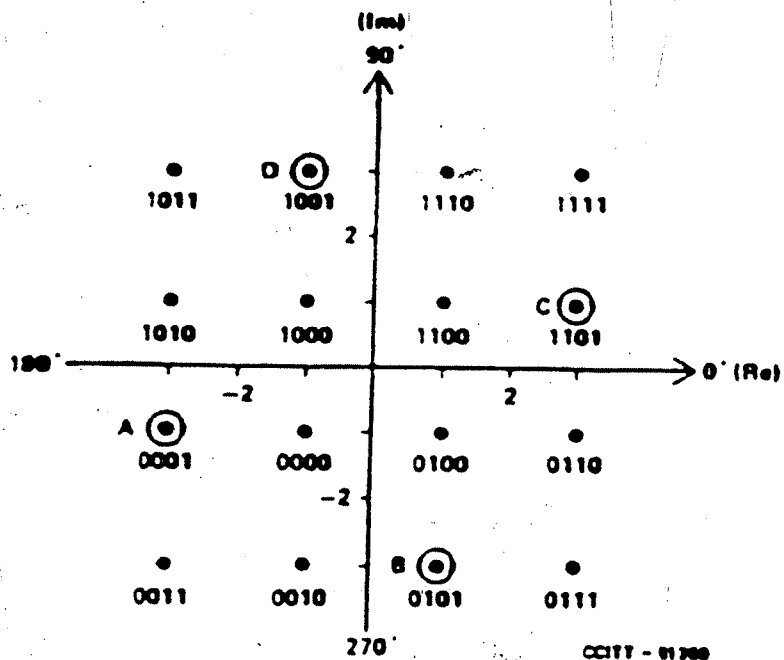


Figure 5.2 Geometrical representation of PAM signal sets.



Los numeros binarios representan $Y1_n, Y2_n, Q3_n, Q4_n$

FIGURA 1/V.32

Constelación de señal de 16 puntos con codificación no redundante para 9600 bit/s y subconjunto A, B, C y D de estados utilizados a 4800 bit/s y para el acondicionamiento

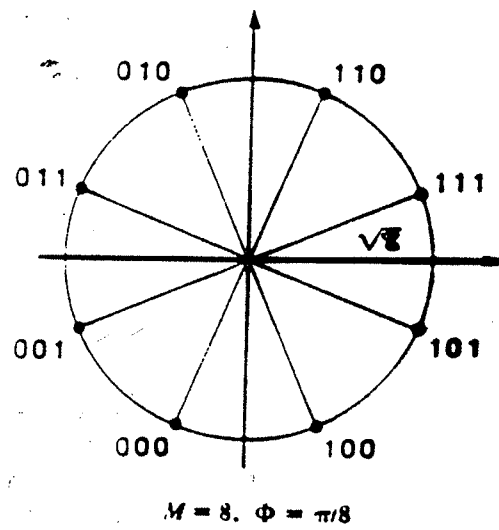
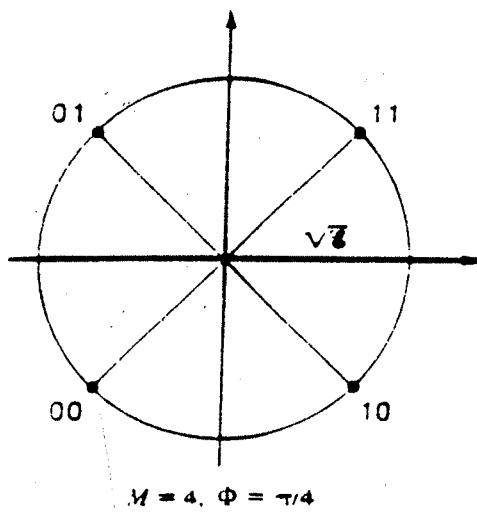
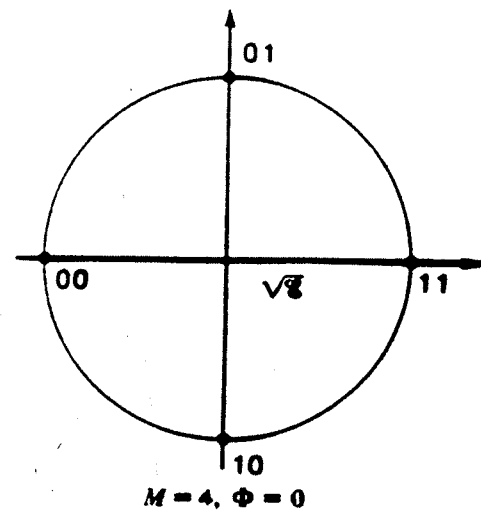
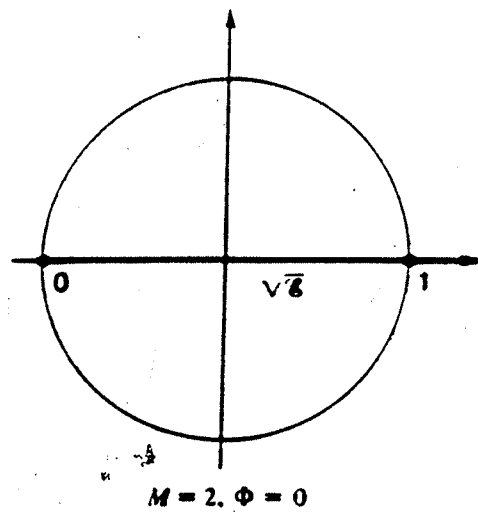


Figure 5.5 Geometrical representation of PSK signal sets.

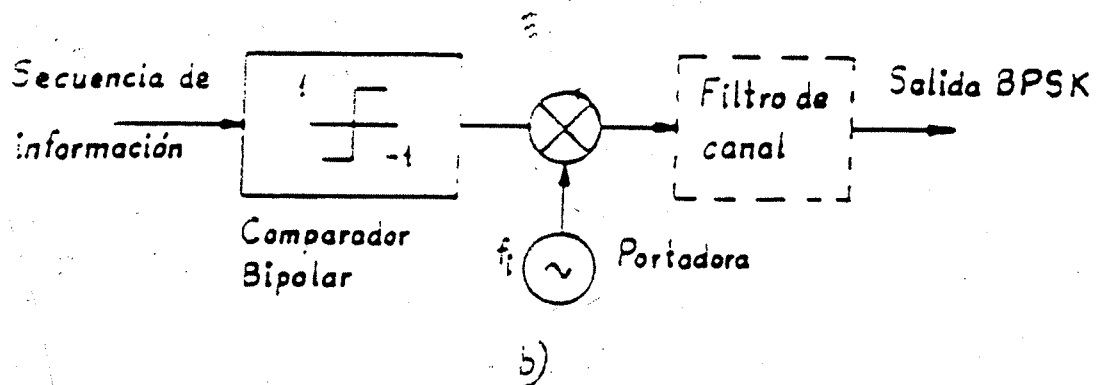
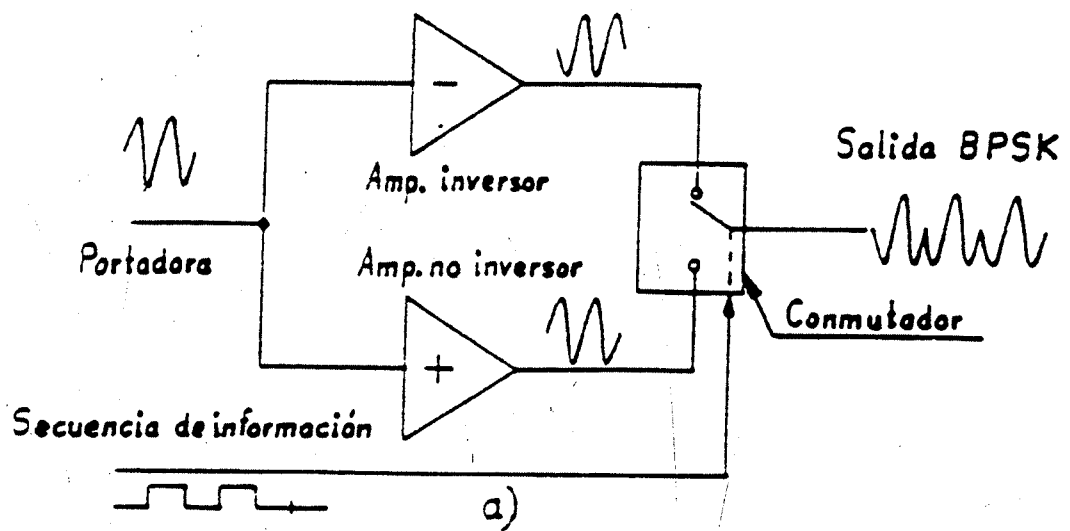


Figura 8.12. Moduladores BPSK.

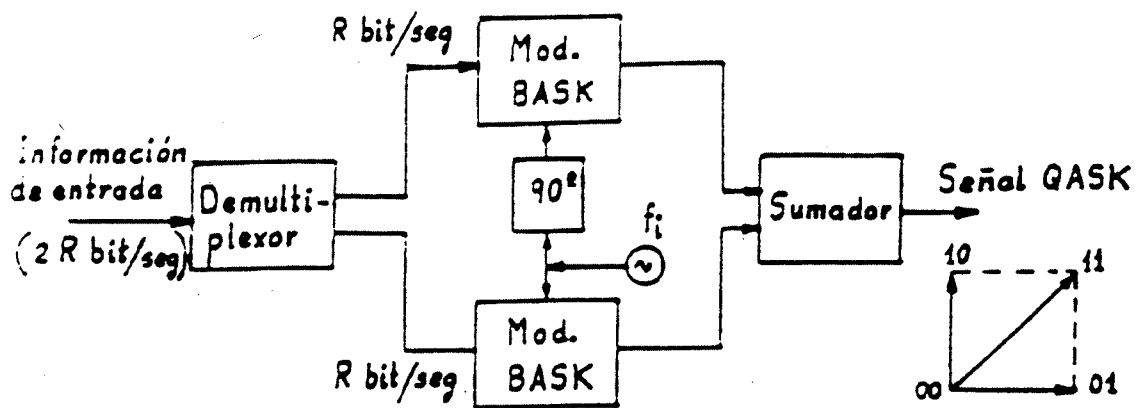


Figura 8.6. Modulador de QASK.

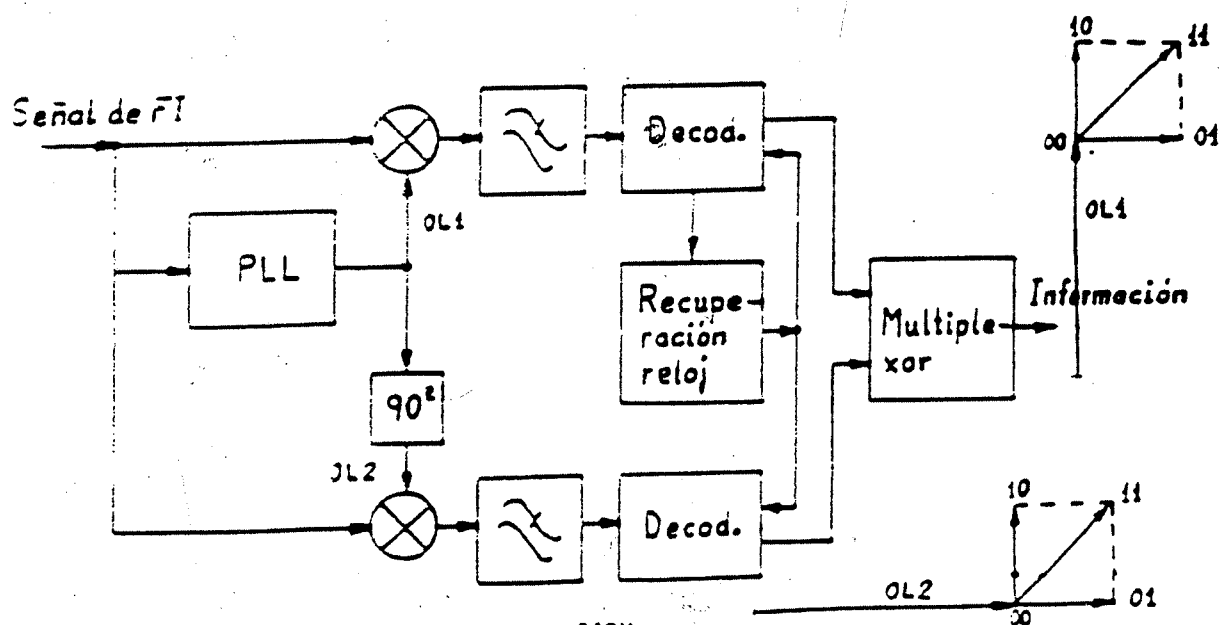


Figura 8.10. Detección coherente de QASK.

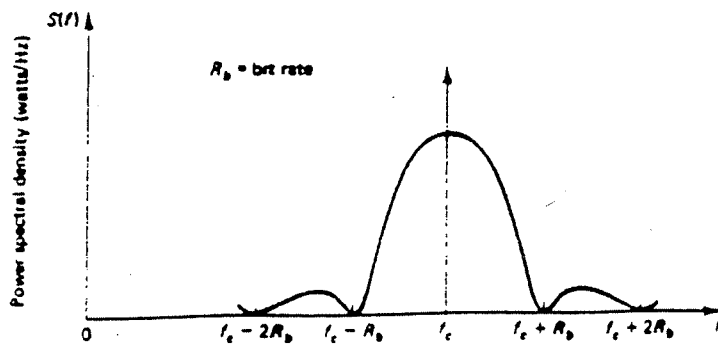


Figure 8.4 Power spectral density of random BASK signal

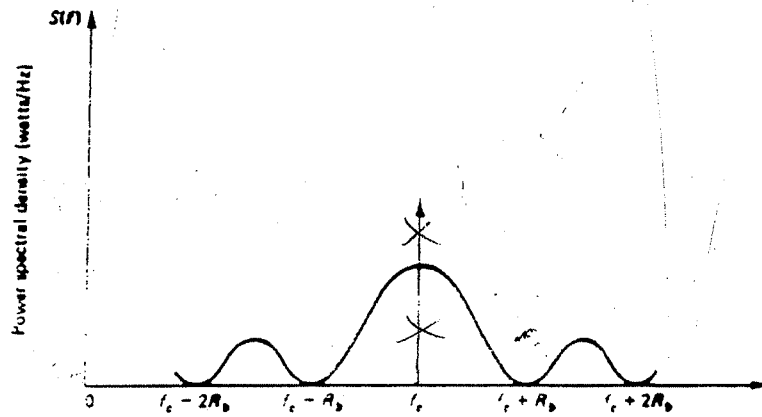


Figure 10.3 Power spectral density of random BPSK waveform

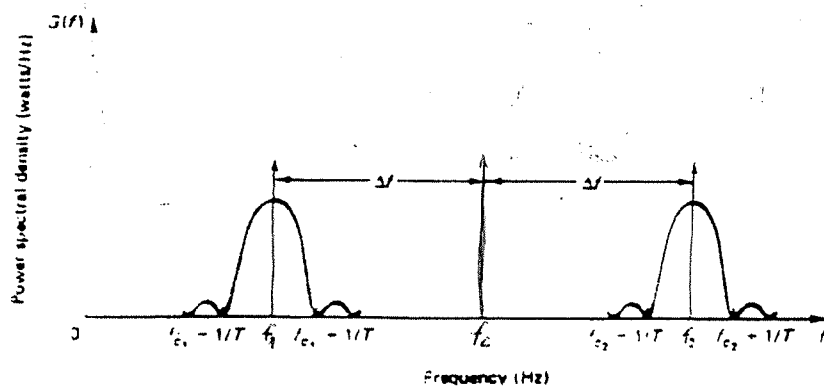


Figure 9.5 Power spectral density of random FSK waveform

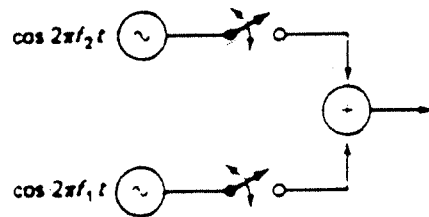


Figure 9.4 FSK as the superposition of two ASK waveforms

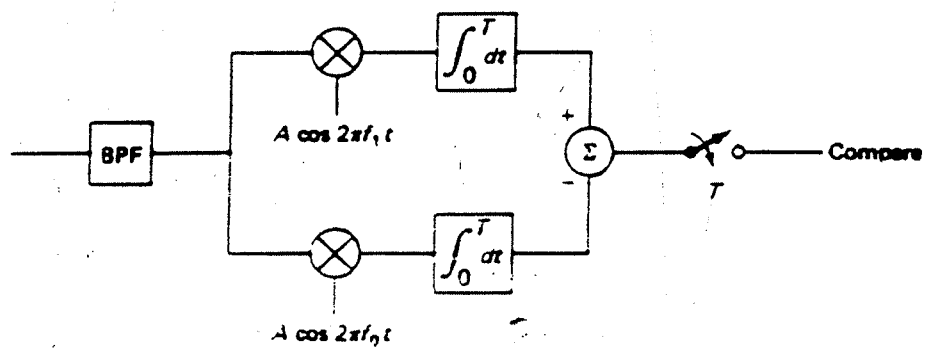


Figure 9.11 Coherent FSK detector

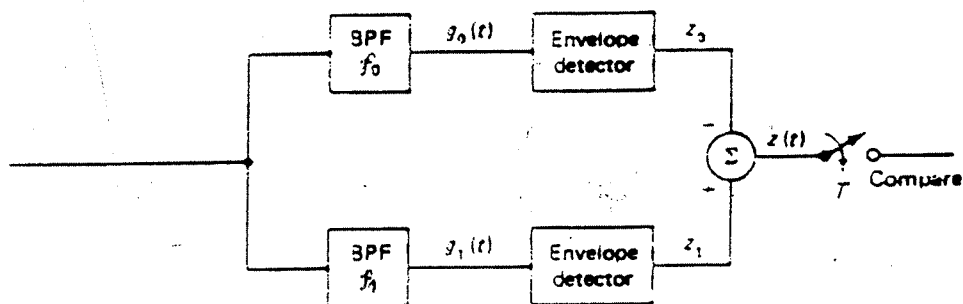


Figure 9.12 Incoherent FSK detector